| MODEL | MAX WEIGHT | AREA cm ${ }^{2}{ }^{(1)}$ | AREA M ${ }^{2}$ |  | FLOOR LOADING $\mathbf{k N / ~ M ~}{ }^{\mathbf{2}}$ |  | POINT LOADING |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Kgs (kN) | FOOT <br> (TYRE) | WORKING <br> (2) | TRANSIT <br> (3) | WORKING <br> (4) | TRANSIT <br> (5) | $\begin{aligned} & \mathrm{kN} / \mathrm{cm}^{2} \\ & \left(\mathbf{k N} / \mathbf{M}^{2}\right) \\ & \text { (6) } \end{aligned}$ | $\begin{aligned} & \hline \text { P.S.I } \\ & \text { (7) } \end{aligned}$ | kN <br> (8) |
| 90 | $\begin{aligned} & 600+120=720 \\ & \mathbf{( 7 . 0 6 )} \end{aligned}$ | 182.4 | $\begin{aligned} & 2.1 \times 2.1= \\ & 4.41 \\ & \hline \end{aligned}$ |  | 1.6 |  | 0.023 (230) | 33 | 4.19 |
| 120M | $1160+200=1360$ <br> (13.34) | 182.4 | $\begin{aligned} & \hline 2.7 \times 2.7= \\ & 7.29 \end{aligned}$ |  | 1.83 |  | 0.043 (430) | 64 | 7.84 |
| 120H | $1300+200=1500$ (14.7) | 324.3 | $\begin{aligned} & 3.36 \times 3.55= \\ & 11.93 \end{aligned}$ |  | 1.23 |  | 0.027 (270) | 39 | 8.75 |
| 120T | $1400+200=1600$ <br> (15.7) | 324.3 | $\begin{aligned} & 3.66 \times 3.55= \\ & 13 \\ & \hline \end{aligned}$ |  | 1.2 |  | 0.029 (290) | 42 | 9.4 |
| 140H | $\begin{aligned} & 1470+225=1696 \\ & (16.63) \end{aligned}$ | 324.3 | $\begin{aligned} & \hline 3.35 \times 3.2= \\ & \mathbf{1 0 . 7 2} \\ & \hline \end{aligned}$ |  | 1.55 |  | 0.031 (310) | 45 | 10.05 |
| 170M | $\begin{aligned} & 1900+200=2100 \\ & \mathbf{( 2 0 . 6 )} \end{aligned}$ | 324.3 | $\begin{aligned} & \hline 4.4 \times 4.25= \\ & 18.7 \\ & \hline \end{aligned}$ |  | 1.1 |  | 0.038 (380) | 55 | 12.3 |
| 170MBE | $2000+200=2200$ <br> (21.58) | 324.3 | $\begin{aligned} & 4.4 \times 4.25= \\ & 18.7 \\ & \hline \end{aligned}$ |  | 1.15 |  | 0.04 (400) | 58 | 12.97 |
| 170H | $1900+200=2100$ <br> (20.6) | 540 | $\begin{aligned} & 4.425 \times 4.37= \\ & 19.34 \end{aligned}$ |  | 1.07 |  | 0.023 (230) | 33 | 12.42 |
| 170HBE | $2000+200=2200$ <br> (21.58) | 540 | $\begin{aligned} & 4.425 \times 4.37= \\ & 19.34 \end{aligned}$ |  | 1.12 |  | 0.024 (240) | 35 | 12.96 |
| 170SD 2WD | $2450+200=2650$ <br> (26) | 540 (504) | $\begin{aligned} & 4.425 \times 4.37= \\ & 19.34 \end{aligned}$ | $\begin{aligned} & 2.4 \times 1.55= \\ & (3.72) \end{aligned}$ | 1.34 | (7.0) | 0.029 (290) | 42 (45) | 15.66 |
| 170SD 4WD | $2775+200=2975$ <br> (29.18) | 540 (504) | $\begin{aligned} & 4.425 \times 4.37= \\ & 19.34 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.4 \times 1.55= \\ & \mathbf{( 3 . 7 2 )} \\ & \hline \end{aligned}$ | 1.51 | (7.85) | 0.0324 (324) | 47 (45) | 17.5 |
| HR10 | $\begin{aligned} & 1930+200=2130 \\ & \text { (20.9) } \end{aligned}$ | (258) |  | $\begin{aligned} & 1.8 \times 1.5= \\ & 2.7 \end{aligned}$ |  | 7.74 | 0.049 (490) | 70 | 12.64 |
| HR10 <br> (SOLID TYRE) | $\begin{aligned} & 1930+200=2130 \\ & \mathbf{( 2 0 . 9 )} \end{aligned}$ | (70) |  | $\begin{aligned} & 1.8 \times 1.5= \\ & 2.7 \\ & \hline \end{aligned}$ |  | 7.74 | 0.1805 (1805) | 258 | 12.64 |
| HR10N | $2150+200=2350$ <br> (23.05) | (258) |  | $\begin{aligned} & 1.8 \times 1.4= \\ & 2.52 \\ & \hline \end{aligned}$ |  | 9.15 | 0.054 (540) | 78 | 13.9 |
| HR12 | $2400+200=2600$ <br> (25.5) | (383) |  | $\begin{aligned} & 1.8 \times 1.8= \\ & 3.24 \end{aligned}$ |  | 7.87 | 0.04 (400) | 58 | 15.32 |
| HR12N | $\begin{aligned} & 2950+200=3150 \\ & \mathbf{( 3 0 . 9 )} \end{aligned}$ | (383) |  | $\begin{aligned} & 1.8 \times 1.5= \\ & 2.7 \\ & \hline \end{aligned}$ |  | 11.44 | 0.048 (480) | 70 | 18.38 |
| HR12N <br> (SOLID TYRE) | $\begin{aligned} & 3022+200=3222 \\ & \mathbf{( 3 1 . 6 )} \end{aligned}$ | (70) |  | $\begin{aligned} & 1.8 \times 1.5= \\ & 2.7 \\ & \hline \end{aligned}$ |  | 11.7 | 0.262 (2628) | 384 | 18.44 |
| HR15N | $6250+225=6475$ <br> (63.5) | (340) |  | $\begin{aligned} & 1.85 \times 1.5= \\ & 2.775 \end{aligned}$ |  | 22.88 | 0.112 (1120) | 162 | 38.08 |

$\left.\begin{array}{|l|l|l|l|l|l|l|l|l|}\hline \text { HR15 4X4 } & \begin{array}{l}5560+225=5785 \\ (\mathbf{5 6 . 7 5 )}\end{array} & (256) & 1.85 X 1.98= \\ \mathbf{3 . 6 6 3}\end{array}\right)$

Note! The point loadings of all trailer units can be altered as desired by the use of larger pads under the jack feet, or spreader plates. For example, if a figure of $50 \mathrm{kN} / \mathbf{M}^{2}$ is quoted as the target point loading, and the intended machine is a $\mathbf{1 2 0 M}$, then dividing the actual figure of $\mathbf{4 3 0}$ by $\mathbf{5 0}$ gives a ratio of 8,6 . Hence the existing foot plate of $182.4 \mathbf{~ c m}^{2}$ needs to increase by this factor to reduce the point loading to the desired figure. Hence $182.4 \times 8.6$ gives an area of $1568 \mathrm{~cm}^{2}$. This would then be divided by $\operatorname{Pi}(3.1416)$ and the result square rooted to give a radius of 22.34 cm . Therefore a circular plate is required, minimum diameter of 447 mm , under each foot. This may be made from substantially thick plywood or metal, so long as the plate itself is capable of transmitting the load over the chosen area. Using a material of insufficient stiffness makes little difference to the initial point loading, i.e. will not work as a load spreader.

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[^0]:    ${ }^{(1)}$ Area of Foot plate is indicated where a machine has outriggers, self-propelled machines show the tyre area in brackets.
    ${ }^{(2)}$ The working area is the machine footprint, in the case of trailer units it is over the foot plate outside edges.
    ${ }^{(3)}$ The transit area for a self-propelled machine is the wheelbase multiplied by the overall transit width.
    ${ }^{(4)}$ Working area loadings are given for trailer units, and are the weight of the machine and operator(s) divided by the floor area of the machine when jacked to the extreme.
    ${ }^{(5)}$ Transit area loadings are given for self-propelled machines and are the weight of the machine and operator(s) divided by the transit area. This loading applies to the machine when the booms are stowed.
    ${ }^{(6)}$ Point loadings are given in all cases. They are the total weight of the machine and operator(s), supported on the area of one foot or tyre and multiplied by a factor of $\mathbf{6 0 \%}$. We have found this to be a very close approximation to the Realistic Point Loading figure, and can be worked to as an absolute. If additional factors of safety are required they should be added to this figure.
    ${ }^{(7)}$ Multiply P.S.I by 144 to give $\mathbf{l b s} / \mathbf{f t}^{2}$, i.e., $82 \mathrm{psi}=11808 \mathrm{lbs} / \mathrm{ft}^{2}$.
    ${ }^{(8)}$ The final column gives the point load as a mass, and not as had been calculated before, a pressure. This is gained by multiplying the floor loading pressure in
    column 8 by the area of the foot, or tyre, listed in column 3. To find the load on the foot or tyre in kilograms, convert these back by multiplying the kN figures by 98.1 , rough approximation 100 . (i.e. the first number shown is 4.19 kN , or 419 kg .)
    ${ }^{(9)}$ The Point load figures for the front and rear axles are measured values, and were obtained from a specific load test.
    No figures are entered for the Niftylift V100, V105 or V125 machines as they are supported on two jacks and the floor loadings will vary to a much greater degree.

